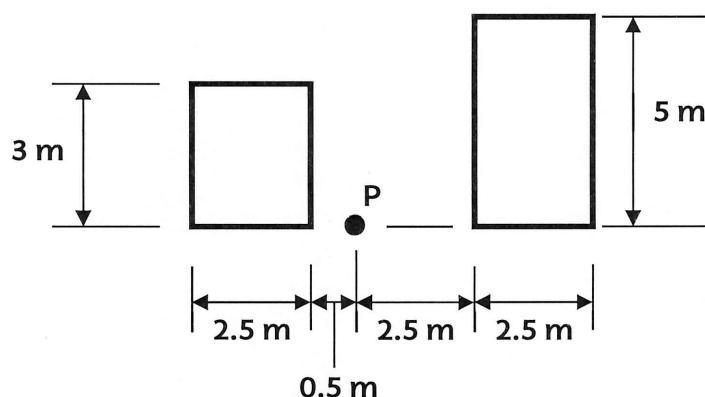
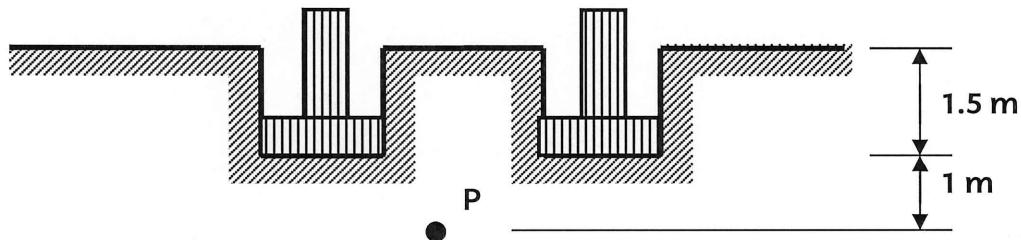


EXERCISE 3

Two footings located 1.5 m below the ground surface (see figure) carry the same uniform load of 110 kN/m^2 . Calculate the vertical stress increment at point P, taking into account both footings.

Additional data: unit weight of soil = 20 kN/m^3 .



Answer: $\Delta\sigma_v = 8.96 \text{ kN/m}^2$.

This load case corresponds to a uniform load on a rectangular area (slides 14 to 17 in the lecture material). According to theory of elasticity, the vertical stress increment at point P will be, taking into account both footings,

$$\Delta\sigma_{vp} = \Delta\sigma_{vp}(\text{left footing}) + \Delta\sigma_{vp}(\text{right footing})$$

$$\Delta T_{vp} (\text{left footing}) = q_{NET_L} \cdot I_{LEFT}$$

where q_{NET_L} is the net load applied by the left footing, and

I_{LEFT} is the influence coefficient (slide 35 of the lecture material) of the left footing

q_{NET_L} is calculated as follows

$$q_{NET_L} = q_L - j \cdot H_{exc} = 110 - 20 \cdot 1,5 = 80 \text{ kN/m}^2$$

I_{LEFT} This coefficient is determined using the chart in slide 15 or the table in slide 16, but taking into account that chart and table can only be used when point P is beneath a corner of the bad area. As, in our case, point P is not beneath a corner, it is necessary to build the real rectangular bad area as an addition/subtraction of rectangular areas, as follows:

$$I_{LEFT} = I_{ACPD} - I_{BCPE}$$

where both rectangles keep to the condition.

$$I_{ACPD} : a = 3 \text{ m}, b = 3 \text{ m}, z = 1 \text{ m}$$

$$m = \frac{a}{2} = \frac{3}{2} = 1.5 ; n = \frac{b}{2} = \frac{3}{2} = 1.5$$

$$\Rightarrow (\text{in Table}) \rightarrow I_{ACPD} = 0.244$$

$$I_{BCPE} : a = 0.5 \text{ m}, b = 3 \text{ m}, z = 1 \text{ m}$$

$$m = \frac{a}{2} = \frac{0.5}{2} = 0.25 ; n = \frac{b}{2} = \frac{3}{2} = 1.5 \Rightarrow I_{BCPE} = 0.137 \text{ (in Table)}$$

$$\text{Then, } I_{LEFT} = 0.244 - 0.137 = 0.107$$

Substituting q_{NET_L} and I_{LEFT}

$$\Delta T_{vp} (\text{left footing}) = 80 \cdot 0.107 = 8.56 \text{ kN/m}^2$$



A similar procedure is taken for the right footing.

$$\Delta \sigma_{vp}(\text{right footing}) = q_{NETR} \cdot I_{RIGHT}$$

$$q_{NETR} = q_R - \gamma \cdot H_{exc} = 110 - 20 \cdot 1.5 = 80 \text{ kN/m}^2$$

$$\boxed{I_{RIGHT}}$$

$$I_{RIGHT} = I_{FHJP} - I_{FGIP}$$

$$\underline{I_{FHJP}}: a=5\text{m}, b=5\text{m}, z=1\text{m}$$

$$m = \frac{a}{z} = \frac{5}{1} = 5; n = \frac{b}{z} = \frac{5}{1} = 5$$

$$\Rightarrow I_{FHJP} = 0.249 \text{ (h Table)}$$

$$\underline{I_{FGIP}}: a=2.5\text{m}, b=5\text{m}, z=1\text{m}$$

$$m = \frac{a}{z} = \frac{2.5}{1} = 2.5; n = \frac{b}{z} = \frac{5}{1} = 5 \Rightarrow I_{FGIP} = 0.244 \text{ (h Table)}$$

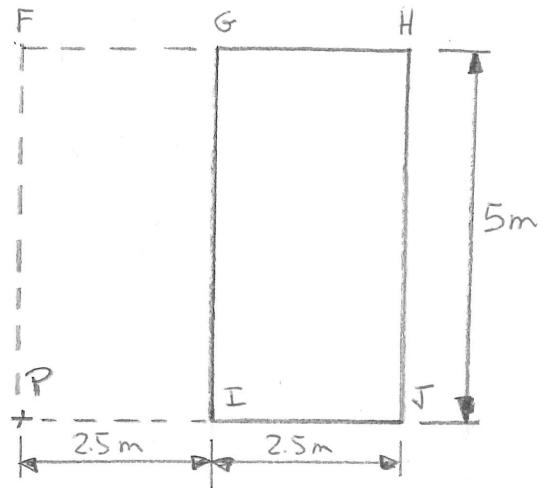
$$\text{Then, } I_{RIGHT} = 0.249 - 0.244 = 0.005$$

Substituting q_{NETR} and I_{RIGHT}

$$\Delta \sigma_{vp}(\text{right footing}) = 80 \cdot 0.005 = 0.4 \text{ kN/m}^2$$

And finally, the vertical stress increment at point P, due to both footings, will be

$$\underline{\underline{\Delta \sigma_{vp}}} = 8.56 + 0.4 = \underline{\underline{8.96 \text{ kN/m}^2}}$$



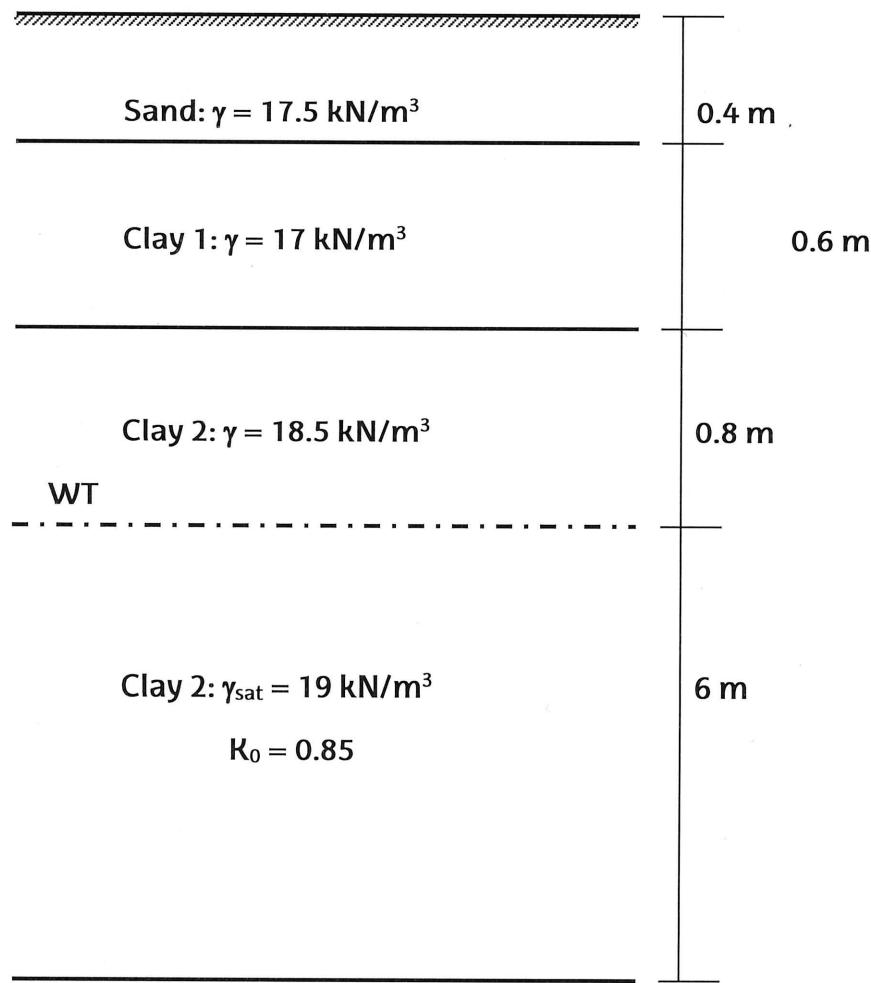
EXERCISE 7

A civil engineering project is to be constructed in an area where the ground surface is horizontal (see figure). A rectangular foundation located 3 m below the ground surface will be used to transfer the construction load uniformly.

- At the pre-construction phase, calculate and plot Mohr circles of total and effective stresses at any point of the soil mass 3 m below the ground surface.

Assuming that a 3 m by 3.4 m rectangular foundation will carry a uniform load of 115 kN/m², determine, at the post-construction phase:

- Total vertical stress at points 0 m and 1 m below the centre of the foundation.



Answers:

- $\sigma_v = 54.8 \text{ kN/m}^2$; $u = 11.76 \text{ kN/m}^2$; $\sigma'_v = 43.04 \text{ kN/m}^2$; $\sigma'_H = 36.58 \text{ kN/m}^2$; $\sigma_H = 48.34 \text{ kN/m}^2$.
- $\sigma_v(0 \text{ m}) = 115 \text{ kN/m}^2$; $\sigma_v(1 \text{ m}) = 126.78 \text{ kN/m}^2$.



1) Pre-construction phase.

In order to determine Mohr circles at point P, it is necessary to calculate σ_v , u , σ'_v , σ'_h and τ_h .

At this point, slides 6 to 9 of the lecture material will be used.

$$\sigma_v = \sum \gamma_i \cdot h_i = 17.5 \cdot 0.4 + 17 \cdot 0.6 + 18.5 \cdot 0.8 + 19 \cdot 1.2 = 54.8 \text{ kN/m}^2$$

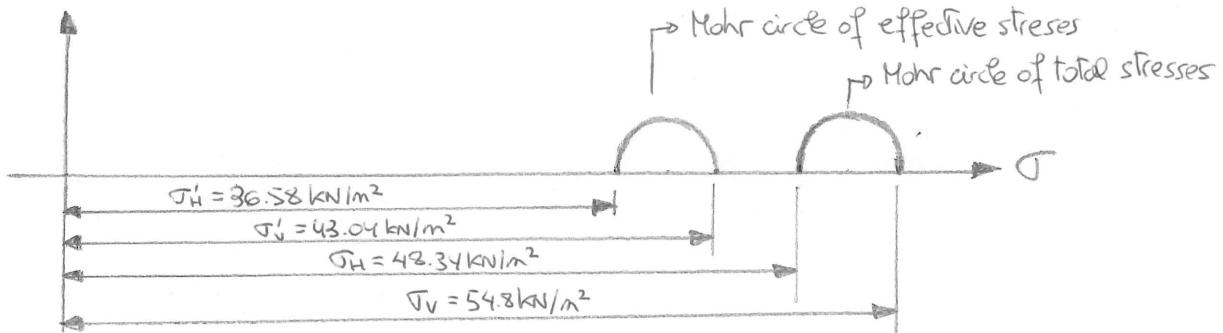
$$u = \gamma_w \cdot h_{WT} = 9.8 (3 - (0.4 + 0.6 + 0.8)) = 11.76 \text{ kN/m}^2$$

$$\sigma'_v = \sigma_v - u = 54.8 - 11.76 = 43.04 \text{ kN/m}^2$$

$$\sigma'_h = K_o \cdot \sigma'_v = 0.85 \cdot 43.04 = 36.58 \text{ kN/m}^2$$

$$\tau_h = \sigma'_h + u = 36.58 + 11.76 = 48.34 \text{ kN/m}^2$$

These values are taken to plot Mohr circles.



2) Rectangular footing : $B=3\text{m}$, $L=3.4\text{m}$, $q=115\text{ kN/m}^2$. Located 3 m below the ground surface.

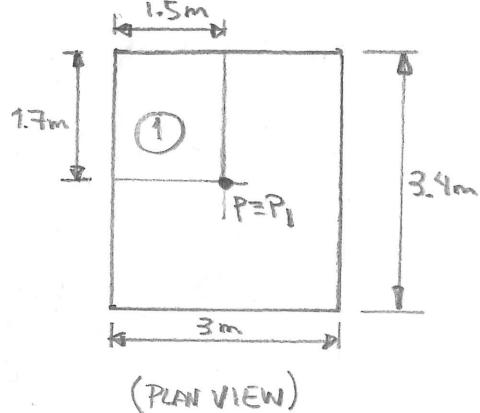
Then, foundation is braced onto the plane where point P is.

$\left. \begin{array}{l} \sigma_v(P) \\ \sigma_v(P_1) \end{array} \right\}$ at the post-construction phase are asked, where points P and P_1 are below the centre of the foundation.

After the load has been applied, the vertical stress increment at points P and P_1 will be

$$\Delta \sigma_v(P) = q_{NET} \cdot I_p$$

$$q_{NET} = q - \gamma \cdot H_{exc} = 115 - [17.5 \cdot 0.4 + 17 \cdot 0.6 + 18.5 \cdot 0.8 + 19 \cdot 1.2] = 60.2 \text{ kN/m}^2$$



$$I_p \stackrel{(1)}{=} 4 \cdot I_p$$

$$I_p \stackrel{(1)}{=} ; a = 1.7, b = 1.5, z = 0 \Rightarrow m = \frac{a}{z} = \frac{1.7}{0} = \infty; n = \frac{b}{z} = \frac{1.5}{0} = \infty \Rightarrow$$

$$\Rightarrow I_p \stackrel{(3)}{=} 0.25 \text{ (from chart slide 15)}$$

$$\Rightarrow I_p \stackrel{(1)}{=} 4 \cdot I_p \stackrel{(3)}{=} 4 \cdot 0.25 = 1 \Rightarrow \Delta \sigma_v(P) = 60.2 \cdot 1 = 60.2 \text{ kN/m}^2$$

$$\Delta \sigma_v(P_1) = q_{NET} \cdot I_{P_1}, \text{ where } q_{NET} \text{ is unique, so } q_{NET} = 60.2 \text{ kN/m}^2$$

$$I_{P_1} \stackrel{(1)}{=} 4 \cdot I_{P_1}$$

$$I_{P_1} \stackrel{(1)}{=} ; a = 1.7, b = 1.5, z = 1 \Rightarrow m = \frac{a}{z} = \frac{1.7}{1} = 1.7; n = \frac{b}{z} = \frac{1.5}{1} = 1.5 \Rightarrow$$

$$\Rightarrow I_{P_1} \stackrel{(3)}{=} 0.220 \text{ (approximately, from chart or table, slides 15 and 16)}$$

$$\Rightarrow I_{P_1} \stackrel{(1)}{=} 4 \cdot I_{P_1} \stackrel{(3)}{=} 4 \cdot 0.220 = 0.88 \Rightarrow \Delta \sigma_v(P_1) = 60.2 \cdot 0.88 = 52.98 \frac{\text{kN}}{\text{m}^2}$$

$$\underline{\sigma_v(P)} = \sigma_v(P) + \Delta \sigma_v(P) = 54.8 + 60.2 = \underline{\underline{115 \text{ kN/m}^2}}$$

at the pre-construction phase

$$\sigma_v(P_1) = \sum \gamma_i \cdot h_i = 17.5 \cdot 0.4 + 17 \cdot 0.6 + 18.5 \cdot 0.8 + 19 \cdot (1.2 + 1) = 73.8 \text{ kN/m}^2$$

$$\underline{\sigma_v(P_1)} = \sigma_v(P_1) + \Delta \sigma_v(P_1) = 73.8 + 52.98 = 126.78 \text{ kN/m}^2$$